

Completeness of the Characteristic Mode Expansion

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Characteristic modes (CM)

- Developed in the 70s by Garbacz, Turpin, Harrington, Mautz [HM71].
- Provides physical understanding and complements simulation and optimization driven antenna design.
- Modes (electric current) determined by the geometry (here lossless).
- Scattering properties, resonances, antenna feed placement, ...
- Generalized eigenvalue problem $XI_n = \lambda_n R_r I_n$, where $Z = R_r + jX$ denotes the MoM impedance matrix.
- ► Orthogonal far fields $\mathbf{I}_m^{\mathsf{H}} \mathbf{R}_r \mathbf{I}_n = \delta_{mn}$ and reactance $\mathbf{I}_m^{\mathsf{H}} \mathbf{X} \mathbf{I}_n = \lambda_n \delta_{mn}$.



First three modes for a rectangle. Only a few dominant modes (small $|\lambda_n|$) for electrically small structures.

Expansion of a current density in characteristic modes

Expansion of a current density

$$\mathbf{I} = \sum_{n=1}^N \alpha_n \mathbf{I}_n \quad \text{and } \mathbf{J}(\mathbf{r}) = \sum_{n=1}^N \alpha_n \mathbf{J}_n(\mathbf{r})$$

Diagonalization of the MoM equation $\mathbf{Z}\mathbf{I}=\mathbf{V}$

$$\sum_{n} \alpha_{n} \mathbf{I}_{n}^{\mathsf{T}} \mathbf{Z} \mathbf{I}_{n} = \alpha_{n} (1 + j\lambda_{n}) = \mathbf{I}_{n}^{\mathsf{T}} \mathbf{V} \to \alpha_{n} = \frac{\mathbf{I}_{n}^{\mathsf{T}} \mathbf{V}}{1 + j\lambda_{n}}$$

When can one expand currents in CM, convergence, theory, practice?

- Always possible for matrices. This is a general property for finite dimensional cases.
- What happens in the (continuous) infinite operator case?



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Efficient and accurate evaluation of \mathbf{R}_{r}

The real-valued part of the impedance matrix with elements

$$Z_{pq} = jk\eta_0 \int_{\Omega} \int_{\Omega} \boldsymbol{\psi}_p(\boldsymbol{r}_1) \cdot \mathbf{G}(\boldsymbol{r}_1, \boldsymbol{r}_2) \cdot \boldsymbol{\psi}_q(\boldsymbol{r}_2) \, \mathrm{dS}_1 \, \mathrm{dS}_2$$

is decomposed by expanding the Green dyadic in regular $\mathbf{u}_v^{(1)}$ and out-going $\mathbf{u}_v^{(4)}$ vector spherical waves

$$\mathbf{G}(\boldsymbol{r}_1, \boldsymbol{r}_2) = -\mathrm{j}k \sum_{\upsilon} \mathbf{u}_{\upsilon}^{(1)}(k\boldsymbol{r}_{<}) \, \mathbf{u}_{\upsilon}^{(4)}(k\boldsymbol{r}_{>}),$$

where $v(\tau, \sigma, m, l)$, $r_{<} = r_{1}$ and $r_{>} = r_{2}$ if $|r_{1}| < |r_{2}|$ and so on. Factorization $\mathbf{R}_{r} = \mathbf{S}^{\mathsf{T}}\mathbf{S} = \mathbf{S}^{\mathsf{H}}\mathbf{S}$, where \mathbf{S} has the elements

$$S_{vp} = k \eta_0^{1/2} \int_{\Omega} \boldsymbol{\psi}_p(\boldsymbol{r}) \cdot \mathbf{u}_v^{(1)}(k\boldsymbol{r}) \, \mathrm{dS}.$$

See [Tay+18] and compare with the T-matrix [Kri16], FMM [CRW93], and far-field expansion [GN13] methods.

Computationally efficient CM evaluation

Factorize the radiation matrix $\mathbf{R}_{r} = \mathbf{S}^{\mathsf{T}}\mathbf{S}$ to rewrite the $N_{\psi} \times N_{\psi}$ generalized eigenvalue problem $eig(\mathbf{X}, \mathbf{R}_r)$

$$\mathbf{X}\mathbf{I}_n = \lambda_n \mathbf{R}_r \mathbf{I}_n = \lambda_n \mathbf{S}^\mathsf{T} \mathbf{S} \mathbf{I}_n$$

by moving X to the right-hand side (or use $X + \alpha R_r$ if X is not invertible)

$$\mathbf{I}_n = \lambda_n \mathbf{X}^{-1} \mathbf{S}^\mathsf{T} \mathbf{S} \mathbf{I}_n \implies \mathbf{S} \mathbf{I}_n = \lambda_n \mathbf{S} \mathbf{X}^{-1} \mathbf{S}^\mathsf{T} \mathbf{S} \mathbf{I}_n \implies \mathbf{S} \mathbf{X}^{-1} \mathbf{S}^\mathsf{T} \mathbf{f} = \lambda_n^{-1} \mathbf{f}_n$$

with $\mathbf{f}_n = \mathbf{SI}_n$. Producing the $N_\alpha \times N_\alpha$ eigenvalue problem [Tay+18]

 $\lambda_n^{-1} = \operatorname{eig}(\mathbf{S}\mathbf{X}^{-1}\mathbf{S}^\mathsf{T}) \quad \text{with } \mathbf{I}_n = \lambda_n \mathbf{X}^{-1}\mathbf{S}^\mathsf{T} \mathbf{f}_n$



CM from diagonalization of the T-matrix (I)



Expand in regular
$$\mathbf{u}_v^{(1)}$$
 and outgoing $\mathbf{u}_v^{(4)}$ spherical waves
 $\boldsymbol{E}_{\mathrm{i}} = k\eta_0^{1/2} \sum_v a_v \, \mathbf{u}_v^{(1)}(k\boldsymbol{r})$ and $\boldsymbol{E}_{\mathrm{s}} = k\eta_0^{1/2} \sum_v f_v \, \mathbf{u}_v^{(4)}(k\boldsymbol{r})$

outside a circumscribing sphere [Han88]. Transition matrix

$$\mathbf{f} = \mathbf{T}\mathbf{a}$$

characterizes the scattering properties of the object [Kri16].

Expansion of the incident field in regular spherical waves is written $\mathbf{V} = \mathbf{S}^{\mathsf{T}} \mathbf{a}$, *i.e.*,

$$V_n = \int_{\Omega} \boldsymbol{\Psi}_n(\hat{\boldsymbol{r}}) \cdot \boldsymbol{E}_{i}(\boldsymbol{r}) \, \mathrm{dV} = \sum_{\upsilon} a_{\upsilon} k \eta_0^{1/2} \int_{\Omega} \boldsymbol{\Psi}_n(\hat{\boldsymbol{r}}) \cdot \mathbf{u}_{\upsilon}^{(1)}(k\boldsymbol{r}) \, \mathrm{dV} = \sum_{\upsilon} a_{\upsilon} S_{\upsilon n}$$

CM from diagonalization of the T-matrix (II)

Expansion of the incident field in regular spherical waves $V = S^T a$ substituted into the MoM formula

$$\mathbf{Z}\mathbf{I} = (\mathbf{R}_r + j\mathbf{X})\mathbf{I} = (\mathbf{S}^\mathsf{T}\mathbf{S} + j\mathbf{X})\mathbf{I} = \mathbf{V} = \mathbf{S}^\mathsf{T}\mathbf{a}$$

and multiplication with $\mathbf{S}\mathbf{X}^{-1}$ produces

$$(\mathbf{S}\mathbf{X}^{-1}\mathbf{S}^\mathsf{T}\mathbf{S} + j\mathbf{S})\mathbf{I} = (\mathbf{S}\mathbf{X}^{-1}\mathbf{S}^\mathsf{T} + j\mathbf{1})\mathbf{S}\mathbf{I} = (\mathbf{S}\mathbf{X}^{-1}\mathbf{S}^\mathsf{T} + j\mathbf{1})\mathbf{f} = \mathbf{S}\mathbf{X}^{-1}\mathbf{S}^\mathsf{T}\mathbf{a}.$$

Here it is seen that the transition matrix **T** mapping regular spherical waves to outgoing spherical waves, $\mathbf{f} = \mathbf{T}\mathbf{a}$, is diagonalized by characteristic modes, *i.e.*, $\mathbf{S}\mathbf{X}^{-1}\mathbf{S}^{\mathsf{T}} = \mathbf{F}\mathbf{\Lambda}^{-1}\mathbf{F}^{\mathsf{T}}$ diagonalizes the T-matrix as

$$(\mathbf{\Lambda}^{-1} + j\mathbf{1})\mathbf{F}^{\mathsf{T}}\mathbf{f} = \mathbf{\Lambda}^{-1}\mathbf{F}^{\mathsf{T}}\mathbf{a} \Rightarrow \mathbf{f} = \mathbf{F}(\mathbf{\Lambda}^{-1} + j\mathbf{1})^{-1}\mathbf{\Lambda}^{-1}\mathbf{F}^{\mathsf{T}}\mathbf{a} = \mathbf{F}(\mathbf{1} + j\mathbf{\Lambda})^{-1}\mathbf{F}^{\mathsf{T}}\mathbf{a}$$

This is a short and simple algebraic formulation of Garbacz, Turpin, Harrington, and Mautz original suggestion [HM71].

Spherical PEC shell

The T-matrix and characteristic modes are well known for a PEC spherical shell. Diagonal T-matrix determined from the Mie series giving

$$t_{\tau l} = -\frac{\mathbf{R}_{\tau l}^{(1)}(ka)}{\mathbf{R}_{\tau l}^{(4)}(ka)} = -\frac{\mathbf{R}_{\tau l}^{(1)}(ka)}{\mathbf{R}_{\tau l}^{(1)}(ka) + j \,\mathbf{R}_{\tau l}^{(2)}(ka)} = -\frac{1}{1 - j \,\mathbf{R}_{\tau l}^{(2)}(ka) / \,\mathbf{R}_{\tau l}^{(1)}(ka)}$$

for $\tau = 1, 2$ and $l = 1, 2, \dots$ corresponding to the CM values

$$\lambda_{\tau l} = -\frac{\mathbf{R}_{\tau l}^{(2)}(ka)}{\mathbf{R}_{\tau l}^{(1)}(ka)}$$

where $R_{\tau l}^{(p)}$ denote the radial functions [Han88] defined as $R_{1l}^{(p)} = z_l^{(p)}$ and $R_{2l}^{(p)}(\kappa) = (\kappa z_l^{(p)}(\kappa))'/\kappa$ with $z_l^{(1)} = j_l$, $z_l^{(2)} = n_l$, and $z_l^{(3,4)} = h_l^{(1,2)}$ denoting spherical Bessel, Neumann, and Hankel function, respectively.

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CM excitation $\mathbf{ZI}_n = \mathbf{V}_n$

Excitation (incident field) corresponding to a characteristic mode $\mathbf{I}_n = \lambda_n \mathbf{X}^{-1} \mathbf{S}^{\mathsf{T}} \mathbf{f}_n$ can be written

$$\mathbf{ZI}_n = (\mathbf{S}^\mathsf{T}\mathbf{S} + j\mathbf{X})\lambda_n\mathbf{X}^{-1}\mathbf{S}^\mathsf{T}\mathbf{f}_n = \mathbf{S}^\mathsf{T}(\mathbf{S}\mathbf{X}^{-1}\mathbf{S}^\mathsf{T} + j\mathbf{1})\mathbf{f}_n\lambda_n = \mathbf{S}^\mathsf{T}\mathbf{f}_n(1+j\lambda_n) = \mathbf{V}_n$$

Characteristic modes can be used to expand current densities corresponding to incident waves which can be expanded in regular spherical waves ($\mathbf{a}_n = (1 + j\lambda_n)\mathbf{f}_n$) such as plane waves or near fields with sources supported outside a sphere circumscribing the object.



Expansion in regular waves

Can use large spheres to show that the relevant region divide into sources inside and outside the convex hull of the object.

Can expand in CM if the source region can separated from the object with a hyperplane.

- Size of sphere in ka indicate how many modes are needed to expand the field.
- Related to the number of CMs.
- Also need to consider expansion of the source.





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Spherical (BoR) torus with radius ka = 2 (hole size)



Spherical (BoR) torus with radius ka = 2 (hole size)



Radiation modes

Radiation modes ρ_n are defined by the eigenvalue problem [EG18; GC19; Sch16]

$$\mathbf{R}_{\mathrm{r}}\mathbf{I}_{n} = arrho_{n}\mathbf{R}_{\Omega}\mathbf{I}_{n}$$
 or from an SVD of $\mathbf{S}\mathbf{\Upsilon}^{-1}$

where spherical wave $\mathbf{R}_r = \mathbf{S}^{\mathsf{H}}\mathbf{S}$ and Cholesky $\mathbf{R}_{\Omega} = \boldsymbol{\Upsilon}^{\mathsf{H}}\boldsymbol{\Upsilon}$ decompositions are used.



Exponentially decreasing ρ_n . Are there any $\rho_n = 0$?

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Exponentially decreasing ρ_n . Are there any $\rho_n = 0$? Left yes, right probably not.

Non-radiating currents

The nullspace of $\mathbf{R}_{\mathrm{r}}=\mathbf{S}^{\mathsf{H}}\mathbf{S}~(\mathbf{SI}=\mathbf{0})$ is related to non-radiating currents

Volume distributed current density

$$\boldsymbol{J}_{\mathrm{NR}}(\boldsymbol{r}) =
abla imes (
abla imes \boldsymbol{F}) - k^2 \boldsymbol{F}$$

with a differentiable vector field F produces a field $E = -j\omega\mu F$. Note F = 0 imply $J_{\rm NR} = E = 0$ [DW73; Kri16].

Surface currents [Dev04] are more involved.

- Cavity solutions with PEC boundary create a field with support inside the cavity. Low-dimensional space at the cavity resonance.
- Cancellation from two sources with identical radiation.



Non-radiating currents

Conclusions

- Decomposition of the radiation matrix $\mathbf{R}_{\mathrm{r}} = \mathbf{S}^{\mathsf{T}} \mathbf{S}$
- Diagonalization of the transition matrix
- Excitation in the form of regular waves
- Convergence can be bad for sources inside of a structures
- Non-radiating currents
- Rapid decay of the radiation modes





References I

- [CHE12] M. Capek, P. Hazdra, and J. Eichler. "A method for the evaluation of radiation Q based on modal approach". IEEE Trans. Antennas Propag. 60.10 (2012), pp. 4556–4567.
- [CRW93] R. Coifman, V. Rokhlin, and S. Wandzura. "The Fast Multipole Method for the Wave Equation: A Pedestrian Prescription". IEEE Antennas Propag. Mag. 35.3 (1993), pp. 7–12.
- [CW15] Y. Chen and C.-F. Wang. Characteristic Modes: Theory and Applications in Antenna Engineering. John Wiley & Sons, 2015.
- [Dev04] A. J. Devaney. "Nonradiating surface sources". JOSA A 21.11 (2004), pp. 2216–2222.
- [DW73] A. J. Devaney and E. Wolf. "Radiating and nonradiating classical current distributions and the fields they generate". Phys. Rev. D 8.4 (1973), pp. 1044–1047.
- [EG18] C. Ehrenborg and M. Gustafsson. Physical bounds and radiation modes for MIMO antennas. Tech. rep. LUTEDX/(TEAT-7265)/1–20/(2018). Lund University, 2018.
- [GC19] M. Gustafsson and M. Capek. "Maximum Gain, Effective Area, and Directivity". IEEE Trans. Antennas Propag. (2019), pp. 1–20.
- [GN06] M. Gustafsson and S. Nordebo. "Characterization of MIMO antennas using spherical vector waves". IEEE Trans. Antennas Propag. 54.9 (2006), pp. 2679–2682.
- [GN13] M. Gustafsson and S. Nordebo. "Optimal Antenna Currents for Q, Superdirectivity, and Radiation Patterns Using Convex Optimization". IEEE Trans. Antennas Propag. 61.3 (2013), pp. 1109–1118.
- [Gus+16] M. Gustafsson, D. Tayli, C. Ehrenborg, M. Cismasu, and S. Nordebo. "Antenna current optimization using MATLAB and CVX". FERMAT 15.5 (2016), pp. 1–29.
- [Han88] J. E. Hansen, ed. Spherical Near-Field Antenna Measurements. IEE electromagnetic waves series 26. Peter Peregrinus Ltd., 1988.
- [HM71] R. F. Harrington and J. R. Mautz. "Theory of characteristic modes for conducting bodies". IEEE Trans. Antennas Propag. 19.5 (1971), pp. 622–628.
- [HM72] R. F. Harrington and J. R. Mautz. "Control of radar scattering by reactive loading". IEEE Trans. Antennas Propag. 20.4 (1972), pp. 446–454.
- [Kri16] G. Kristensson. Scattering of Electromagnetic Waves by Obstacles. SciTech Publishing, an imprint of the IET, 2016.
- [Pfe17] C. Pfeiffer. "Fundamental Efficiency Limits for Small Metallic Antennas". IEEE Trans. Antennas Propag. 65.4 (2017), pp. 1642–1650.
- [Sch16] K. R. Schab. "Modal analysis of radiation and energy storage mechanisms on conducting scatterers". PhD thesis. University of Illinois at Urbana-Champaign, 2016.

References II

- [Tay+18] D. Tayli, M. Capek, L. Akrou, V. Losenicky, L. Jelinek, and M. Gustafsson. "Accurate and Efficient Evaluation of Characteristic Modes". IEEE Trans. Antennas Propag. 66.12 (2018), pp. 7066–7075.
- [Tha18] H. L. Thal. "Radiation efficiency limits for elementary antenna shapes". *IEEE Trans. Antennas Propag.* 66.5 (2018), pp. 2179 –2187.
 [VCF10] J. Volakis, C. C. Chen, and K. Fujimoto. *Small Antennas: Miniaturization Techniques & Applications*. McGraw-Hill, 2010.